

## Dominion & Valley Road Apartments

## **Civil Engineering Report**

for: Precinct Properties New Zealand Limited



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### **DOCUMENT CONTROL**

This report was prepared by Michael Martin and reviewed by Will Djongianto

Respectfully submitted

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### **TABLE OF CONTENTS**

DO	CUME		ii
TAE	BLE O	F CONTENTS	iii
1	INTR	RODUCTION	5
2	EXIS	TING SITE DESCRIPTION	6
	2.1	Site Location and Property Details	6
	2.2	Existing Features	7
	2.3	Topography	7
3	PRO	POSED DEVELOPMENT	8
4	FLOO	OD HAZARDS	9
5	EAR	THWORKS	10
	5.1	General Scope and Methodology	
	5.2	Extent and Quantities	
	5.3	Construction Working Hours and Timeframes	
	5.4	Construction Plant	
	5.5	Construction Access and Vehicle Movements	
	5.6	Erosion and Sediment Controls	
6	STO	RMWATER	16
	6.1	Existing Stormwater	
	6.2	Proposed Stormwater	16
7	WAS	STEWATER	18
	7.1	Existing Wastewater	
	7.2	Proposed Wastewater	
8	WAT	ER SUPPLY	20
	8.1	Existing Water Supply	20
	8.2	Proposed Water Supply	21
9	UTIL	ITY SERVICES	22
	9.1	Power	22
	9.2	Gas	22
	9.3	Communications	22
10	SUM	IMARY AND CONCLUSIONS	23
Арр	licabi	lity and Limitations	25





#### **List of Tables**

Table 1. Site Properties	6
Table 2. Proposed Development Surface Areas	8
Table 3: Estimated Earthworks Quantities	
Table 4. Estimated Vehicle Movements	
Table 5. Pre-Development and Post-Development Surface Areas	
Table 6. Pre-Development and Post-Development Peak Flows	17

#### **List of Figures**

Figure 1. Site Location (from Ashton Michell Architects)	6
Figure 2. Existing Surfaces (from GeoMaps)	7
Figure 3. Bulk Earthworks Extent and Depths	11
Figure 4. Existing Public Wastewater (from GeoMaps)	18
Figure 5. Existing Public Water Network (from GeoMaps)	20

#### List of Appendices

- Appendix A Topographical Survey
- Appendix B Proposed Development Layout
- Appendix C Civil Engineering Drawings
- Appendix D Stormwater Calculations
- Appendix E Soakage Testing
- Appendix F Water and Wastewater Calculations





### **1 INTRODUCTION**

Babbage Consultants Limited (Babbage) have been engaged by Precinct Properties New Zealand Limited (Precinct) to prepare a civil engineering report for the proposed Dominion & Valley Road Apartments, located at the corner of Dominion and Valley Roads, Mount Eden.

This report has been prepared to support a resource consent application for the proposed development and provides information on the civil engineering aspects of the proposed development as follows:

- existing site
- proposed development
- flood hazards
- proposed earthworks and erosion and sediment controls
- stormwater drainage and management
- wastewater drainage and water supply
- utility services

We note this assessment is based on preliminary design information only which will be developed through subsequent design stages.





### **2 EXISTING SITE DESCRIPTION**

#### 2.1 Site Location and Property Details

The site is located at the corner of Dominion Road and Valley Road as shown in Figure 1 below.

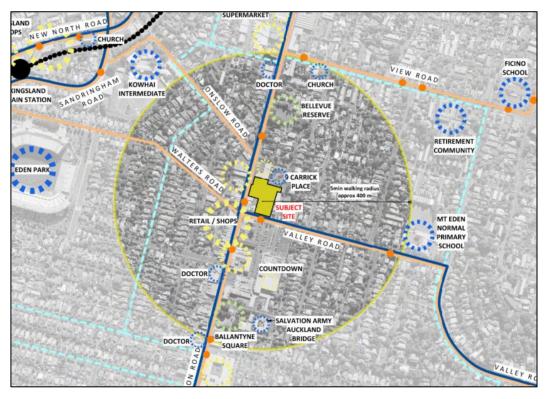


Figure 1. Site Location (from Ashton Michell Architects)

The site consists of four properties as shown on Table 1 below.

#### Table 1. Site Properties

Address	Legal Description
198 - 202 Dominion Road	Lot 1 DP 51797 &
	Pt Lot 4 DP 182
	Pt Lot 5 DP 182
214 - 22 Dominion Road	Lot 2 DP 54203 &
	Pt Lot 1 DP 31896
	Pt Lot 3 Allot 8 SEC 10
113 - 117 Valley Road	Lot 1 DP 54203
	Pt Lot 3 DP1

Refer to Yeoman's Site Survey in **Appendix A** for property locations. The total site area is 5,254 m<sup>2</sup>.

The AUP zonings for the site are Business – Local Centre and Residential – Terrace Housing and Apartment Buildings.





#### 2.2 Existing Features

The existing site development is shown in Figure 2 below.



Figure 2. Existing Surfaces (from GeoMaps)

The existing site is almost entirely covered by existing building roofs and pavements. There are two existing vehicle accessways from Dominion Road, two from Valley Road and one from Carrick Place. There are existing buildings on neighbouring properties at the western end of the northern boundary and the northern end of the eastern boundary.

#### 2.3 Topography

The current ground contours are shown on Yeoman's Site Survey drawings in **Appendix A**. The site measures approximately 95 m from north to south and approximately 70 m from west to east across the central area of the site.

The site generally slopes downwards from the northern boundary to the southern boundary, although there is a low point within a depression in the north-western area of the site, and the southern area of the site is relatively flat.

The existing ground elevation at the north-west corner is approximately RL 55.5 m and at the north-east corner approximately 56.0 m. The existing ground elevation at the south-west corner is approximately RL 52.4 m, and at the south-east corner, approximately 52.5 m. The elevation difference between the northern and southern boundaries, therefore, varies between approximately 3.1 m and 3.5 m. The elevation of the low point within the depression in the north-western area is approximately 51.3 m.





### **3 PROPOSED DEVELOPMENT**

The preliminary layout of the proposed development is illustrated in Ashton Mitchell's Proposed Plan – Level 1, included in Appendix B. The development consists of three, five-storey residential buildings, housing a total of 135 apartments, with a basement carpark extending beneath all three buildings. Retail units are proposed along the Valley Road frontage.

Pedestrian access is proposed from Dominion Road, Valley Road, and Carrick Place, with vehicle access from Valley Road and Carrick Place. The podium level (Level 1) is set at RL 52.25 m, while the basement carpark is at RL 51.85 m, with vehicle access provided from Valley Road. The surface areas for the proposed development are detailed in Table 2 below. Surface areas for the proposed development are shown in Table 2 below.

	Area
Area	(m²)
Building roofs	3,250
External vehicle pavements & Footpaths	957
Landscaping	1,067
Total	5,254





### 4 FLOOD HAZARDS

A separate flood hazard report has been prepared by Babbage to address the implications of the existing flood hazards on the proposed development





### **5 EARTHWORKS**

#### 5.1 General Scope and Methodology

The bulk earthworks will largely consist of excavation for the proposed basement once existing building floor slabs and existing pavement surfacing has been removed.

The maximum bulk excavation depth is estimated to be approximately 1.0 m with some deeper bulk excavation in the north-western corner. We have assumed the depth of excavation will extend to approximately 0.35 m below the basement floor finished floor level. The cut materials from the excavation are to be largely transported and disposed off site.

Some bulk fill, up to approximately 1.0 m thickness, is required in the western and eastern areas of the site. Excavated existing hardfill materials are likely to be used for this bulk fill.

Geotechnical investigations indicate the site is underlain by a capping layer of hardfill and minor cohesive material, then basalt rubble and fractured rock, overlying solid basalt rock. Refer to Initia's Geotechnical Interpretative Report. Bulk excavations are likely to largely within the fill and basalt rubble but will also extend into the solid basalt rock.

The basement excavation will require temporary batters or rock bolts and permanent retaining walls up to approximately 3.6 m in the north-western corner. Refer to Initia's Geotechnical Interpretative Report for details on retaining methods.

Geotechnical investigations also indicate the groundwater level in the basalt rock aquifer is at approximately 20 m below existing ground level and therefore should not be encountered during bulk excavation.

Ground contamination has been assessed in Williamson Water & Land Advisory's (WWLA) Ground Contamination Review, 31 July 2024. This review concluded that existing fill materials on 214 – 222 Dominion Road contain contaminants (metals and hydrocarbons with traces of asbestos) and the same contaminants are likely to be present across the site. WWLA has prepared a contamination Site Management Plan which states that standard earthwork controls are appropriate to mitigate the heavy metals but that further testing will be required during construction to mitigate the hydrocarbon and asbestos contamination.

Bulk excavation of basalt rock may require the use of heavy plant (35 to 50 tonne excavators) or pneumatic breakers. The remaining earthworks is expected to require conventional earthmoving plant and equipment, such as excavators, trucks, compactors and pumps.

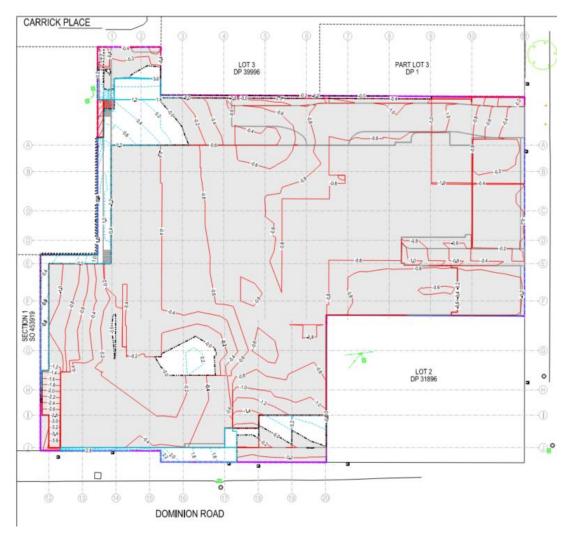




### 5.2 Extent and Quantities

The extent of the proposed earthworks, finished ground levels, subgrade levels and cut and fill depths are shown on the preliminary earthworks drawings included in **Appendix C**.

The approximate extent and depths for the bulk earthworks are shown in Figure 3 below.



#### Figure 3. Bulk Earthworks Extent and Depths

The estimated earthworks quantities for the proposed basement excavation, and carparking and landscaping areas, are provided in Table 3 below.



Table 3: Estimated Earthworks Quantities

Activity	Quantity
Total earthworks area	<b>5,250</b> m <sup>2</sup>
Cut materials:	
<ul> <li>Strip existing asphalt to disposal off site</li> </ul>	200 m <sup>3</sup>
- Bulk cut to bulk fill	300 m <sup>3</sup>
- Bulk cut to disposal off site	<b>2,500</b> m <sup>3</sup>
Total cut materials	<b>3,000</b> m <sup>3</sup>
Fill materials:	
- Bulk cut to bulk fill	300 m <sup>3</sup>
- Import hardfill to building platform and pavements	<b>1,000</b> m <sup>3</sup>
Total fill materials	<b>1,300</b> m <sup>3</sup>

### 5.3 **Construction Working Hours and Timeframes**

High noise generating construction works are proposed to be undertaken during daytime hours. Refer to Marshall Day's Assessment of Acoustic Effects, 28 August 2024.

It is estimated the bulk earthworks construction period would be approximately 2 months.

Erosion and sediment controls would be installed prior to the commencement of bulk earthworks.

#### 5.4 Construction Plant

The anticipated methodology for constructing the earthworks will include the use of the following construction plant:

- Large excavator for rock excavation and/or pneumatic breakers
- Medium and small excavators
- Dump trucks
- Rollers and compactors
- Semi-trailer and 6 wheel trucks
- Generator and pumps
- Other specialist equipment

#### 5.5 Construction Access and Vehicle Movements

The main construction access to the site for the earthworks is expected to be from Valley Road.

The duration for the bulk earthworks is expected to be approximately 2 months, which equates to approximately 9 working weeks. At 5 working days per week, this gives a total of 45 working days for the bulk earthworks for the basement excavation.





The anticipated vehicle movements per day are provided in Table 4 below.

Construction Phase	Vehicle Type	Average vehicles / day	Average trips / day
Bulk Earthworks			
Dispose cut material off site	Semi trailer truck	7.5	15.0
Import hardfill to site	Semi trailer truck	2.8	5.6
Totals		10.3	20.6

#### Table 4. Estimated Vehicle Movements

### 5.6 Erosion and Sediment Controls

The proposed erosion and sediment controls have been designed in accordance with Auckland Council's GD05 and are shown on the drawings in **Appendix C**.

We note the existing volcanic materials are considered to be low sediment generating materials. The proposed measures are described below.

#### **Stabilised Construction Entrance**

A stabilised construction entrance in accordance with the standard detail from Auckland Council's GD05 will be installed at the proposed construction access from Valley Road.

#### **Diversion Measures**

A clean water run off diversion measure, either a bund or sandbags, will be installed along the northern side of the proposed earthworks area to divert clean water run off away from the basement excavation to adjacent pavement areas.

#### **Existing Stormwater Inlet Protection**

There are existing stormwater catch pits within the site and on Valley Road. To mitigate sediment entering these existing catchpits, a silt sock will be placed around the existing catchpits.

#### **Basement Excavation Dewatering**

Sediment laden water within the basement excavation will be directed to a sump or sumps excavated into the base of the excavation. From the sumps the water will be pumped to existing ground level to multichamber settlement skip bins or a Silt-buster or equivalent device. Clarified water from the settlement skip will be discharged to an existing stormwater soakpit.

#### Dust Control

As the earthworks are largely associated with a basement excavation, dust nuisance to surrounding areas is expected to be significantly less than a large, open elevated site. Dust generation will be monitored by the contractor and dust will be controlled by water sprays or proprietary dust suppressant sprays.





#### Stockpiles

It is likely that most materials will be cut and loaded directly off site rather than being stockpiled on site. Erosion and sediment control for any temporary stockpiles of sediment generating materials will be managed in accordance with GD05. This will include:

- Installing super silt fence as required.
- Limiting the average height to less than 2.5 m.

#### Site Stabilisation

The basement excavation is to be stabilised progressively, by the placement of hardfill over the base of the excavation. Other areas are also to be progressively stabilised either by the placement of hardfill or placement of topsoil and grassing.

#### Monitoring and Maintenance

Monitoring and maintenance are to be carried out generally in accordance with GD05 and consists of:

- Weekly monitoring and recording of status of ESC control measures.
- Monitoring immediately before and after any significant rainfall event.
- Immediate repair of any defects in ESC control measures.
- Monitoring of any change in catchment areas through the progress of the works.
- Cleaning out of accumulated sediment from devices when 20% full.
- Preparation of contingency provisions for main ESC measures, e.g. mulching if grassing not complete.
- Decommission only after stabilisation of upstream catchment.

#### Earthworks Construction Management Plan

An Earthworks Construction Management Plan will be prepared by the contractor and submitted to Auckland Council for certification prior to commencement of the earthworks.

This plan will include detailed information on:

- General site management.
- Council communications and approvals.
- Engineer's communications and certification.
- Earthworks construction timeframes and staging.
- Earthworks construction methodology:
  - Site access and traffic management.
  - Work hours.
  - Off site disposal site(s).





- Plant, equipment and personnel.
- Protection of existing property and services.
- Excavation support or instability control.
- Hazardous substance spill protection.
- Dust control.
- Erosion and sediment control measures.
- Accidental discovery (cultural, archaeological, etc).
- Contamination management.
- Site stabilisation.
- Site reinstatement methodology.
- Earthworks and sediment control monitoring.





### 6 STORMWATER

#### 6.1 Existing Stormwater

#### **Existing Impervious Areas**

The existing site consists almost entirely of impermeable surfaces with approximately 3,100 m<sup>2</sup> of roofs and 2,150 m<sup>2</sup> of pavements. There is a small area of existing landscaping which is approximately 24 m<sup>2</sup>.

#### **Existing Primary and Secondary Flows**

Primary (10 year) stormwater discharges to existing on-site rock bore soakpits but they are limited in number and likely to be in poor condition. The soakpits discharge to the underlying volcanic aquifer.

Secondary (100 year) stormwater ponds in the low point in the north-west area of the site and then discharges south to Valley Road.

We have calculated the existing 10 year and 100 year peak flows from the site using TP108 method. (with 3.8 degrees climate change) at 31 l/s and 86 l/s, respectively. The calculations are presented in **Appendix D**.

#### **Existing Stormwater Quality**

There is no existing stormwater quality treatment in place for vehicle pavements

#### 6.2 Proposed Stormwater

#### **Proposed Impervious Areas**

The proposed site will have a significant reduction in impervious surfaces from the pre-development of approximately 100% to post-development of approximately 80%. The pre-development and post-development surface areas are shown in Table 5 below.

Area	Pre-Development (m²)	Post-Development (m²)
Impervious Areas:		
Building roofs	3,100 (59%)	3,250 (62%)
Exposed pedestrian and vehicle pavements	2,150 (41%)	957 (18%)
Pervious Areas:		
Landscaping	24 (0.5%)	1,067 (20%)
Total	5,274 (100%)	5,274 (100%)

Table 5. Pre-Development and Post-Development Surface Areas

#### **Proposed Primary and Secondary Flows**

We have calculated the proposed 10 year and 100 year peak flows from the site. These have been calculated using TP108 method including 3.8 degrees climate change in accordance with the Auckland



Council's draft Stormwater Code of Practice, Version 4. The post-development flow rates are compared to the pre-development peak flow rates in Table 6 below. The preliminary flow calculations are presented in **Appendix D**.

Storm Event	Pre-Development	Post-Development
10 year	119 l/s	105 l/s
100 year	219 l/s	203 l/s

Table 6. Pre-Development and Post-Development Peak Flows

Primary (10 year) stormwater flows are to discharge to on-site rock bore soakpits to the underlying volcanic aquifer. The new soakpits will have pre-treatment via sumps prior to discharge and be designed in accordance with Auckland Council's GD07.

Soakage testing was completed by Tonkin & Taylor in 2017 for the previous Eke Panuku development in two boreholes on the site which resulted in soakage rates of approx. 35 l/s in each borehole. T&T recommended a design soakage rate of 27 l/s. For soakpits with two boreholes, this equates to a total of 3 soakpits proving a total disposal flow of approximately 140 l/s.

To reduce secondary (100 year) stormwater flows and volumes it is also proposed to discharge 33% (or 33 l/s) of the secondary flow to ground soakage. This would be provided by an additional soakpit with two boreholes. The balance of the secondary flows would discharge to Dominion Road and Valley Road.

The preliminary stormwater drainage for the site is shown on the preliminary civil drawings in **Appendix C**.

#### Stormwater Quality

Stormwater quality treatment in accordance with Auckland Council's GD01 is proposed for the approximately 320  $m^2$  of exposed vehicle access pavements in the eastern area of the site prior to discharge to the on-site soakpits.

Stormwater from building roofs is to be discharged via catchpits prior to discharge to the on-site soakpits. Soakpits will be fitted with filter cages in accordance with Auckland Council's GD07 which provide pretreatment as gross pollutant traps prior to discharge to the underlying volcanic aquifer.





### 7 WASTEWATER

#### 7.1 Existing Wastewater

Based on the information derived from GeoMaps, there are currently 150 mm and 225 mm public wastewater pipelines traversing across the site and existing public wastewater manholes located within No. 115 Valley Road and No. 200 Dominion Road as shown in Figure 4 below.



Figure 4. Existing Public Wastewater (from GeoMaps)

While not explicitly shown on GeoMaps, it can be assumed that wastewater discharge from the existing development on-site is being discharged into the existing public wastewater system via private lot connections.

As part of the demolition process, all existing private wastewater connections from the existing development on the site are to be disconnected and capped.

There also appears to be existing connections into public manholes from neighbouring properties at 9 Carrick Place (into MH 531376) and 224 – 228 Dominion Road (into MH 531403).

The existing public wastewater layout is also shown on Yeoman's Site Survey drawings in **Appendix A**.





#### 7.2 Proposed Wastewater

#### 7.2.1 Public Wastewater Network

In order to accommodate the proposed building footprint, the majority of the existing public wastewater network within the site is to be relocated around the eastern side of the site. The proposed realignment consists of the decommissioning and removal of the northern public wastewater manhole (MH 531376) on site and the addition of eight new public wastewater manholes. The proposed layout of the relocated public wastewater network is shown the preliminary civil drawings in **Appendix C**.

The western public manhole (MH 531403) is to be retained within the carpark basement to continue to provide connections for the adjacent properties at 224 – 228 Dominion Road. The existing public pipe downstream of MH 531403 is to be bridged by the foundations for the proposed buildings.

#### 7.2.2 Wastewater Generation

Wastewater generation demand for the proposed development has been calculated in accordance with Watercare Code of Practice Section 6.3.5.3. These calculations are provided in **Appendix F**.

This assessment indicates a wastewater peak dry weather flow of 2.3 l/s and a wastewater peak wet weather flow of 3.9 l/s from the proposed development. We note this is significantly lower than the 5.0 l/s for the previously consented development.

#### 7.2.3 Wastewater Network Capacity

In accordance with Watercare Code of Practice for Land Development and Subdivision, capacity assessment of the public wastewater network needs to be undertaken to the nearest downstream 300 mm public pipeline. However, the nearest 300 mm wastewater pipeline located more than 650 m downstream of the proposed development and we consider it more appropriate to undertake a capacity assessment on the section of the public wastewater pipeline immediately downstream of the proposed connection point.

A capacity assessment for this pipeline has been undertaken in accordance with Watercare Code of Practice Section 6.3.5.3. The assessment included topographical survey of the invert level of the first public manhole downstream of the proposed development to provide greater accuracy. The results of the assessment are as shown in the calculations in **Appendix F**. The output of this downstream capacity assessment indicates that the peak wet weather flow from the contributing catchment is 18 l/s which is significantly lower than the capacity of the public wastewater pipe of 52 l/s.





### 8 WATER SUPPLY

#### 8.1 Existing Water Supply

GeoMaps indicates there are existing 100 mm watermains within the eastern berm of Dominion Road and the northern road carriageway of Valley Road, adjacent to the western and southern boundary of the site, respectively. These existing watermains are shown on Figure 5 below.



Figure 5. Existing Public Water Network (from GeoMaps)

There is also a 200 mm watermain within the western berm of Dominion Road, across the road from the site. There are three existing hydrants in close proximity to the site, two in Valley Road at the southern boundary of the site and one in Dominion Road at the western boundary of the site.

The existing buildings on site are currently being serviced by 20 mm lot connections off either of the existing 100 mm public watermains.



#### 8.2 Proposed Water Supply

#### 8.2.1 Water Network Connection

It is proposed to connect to the existing 100 mm watermain in Valley Road on the southern boundary of the site. The proposed connection is shown on the preliminary civil drawings in **Appendix C**.

#### 8.2.2 Potable Water Demand

Potable water demand for the proposed development has been calculated in accordance with Watercare Code of Practice Section 6.3.5.3. These calculations are provided in **Appendix F**.

This assessment indicates a water peak daily demand of  $151 \text{ m}^3$  and a water peak hourly demand of 4.4 l/s from the proposed development.

#### 8.2.3 Firefighting

In accordance with the New Zealand Fire Service Firefighting Water Supplies Code of Practice SNZ PAS 4509:2008, the proposed development is classified under category FHC 1 (for both the apartment units and café). Based on the proposed floor area of less than 599m<sup>2</sup> for each apartment unit and cafe, the water supply classification for the proposed development is expected to be FW3, subject to confirmation from the fire engineer.

Based on the fire water classification of FW3, the reticulated firefighting water supply requirement for the proposed development is 1,500 l/min (25 l/s) of water flow within 135m with an additional 1,500 l/min (25 l/s) within 270m through a maximum number of 3 fire hydrants.

#### 8.2.4 Water Supply Capacity

Based on the size of the existing public mains (100 mm) as part of a closed-loop system, it is expected the existing water supply network will have sufficient capacity for the potable water demand from the proposed development.

Flow and pressure testing is yet to be undertaken to confirm flow and pressure of public water system. On site storage tanks and booster pumps may be needed if pressure and flows are not sufficient for firefighting water supply for the proposed development. We note the firefighting supply is no greater than the previously consented apartment development on the site.





### 9 UTILITY SERVICES

#### 9.1 Power

Based on the information provided by BeforeUDig, there are existing underground 11kV and 400V power lines within the berms of Dominion Road and Valley Road adjacent to the site boundary. There are also existing streetlights and power supply pillars within the berm. As the current usage of the site and the surrounding area includes retail and commercial activities, it is likely that the existing network will have adequate capacity to service the electricity demands of the proposed development.

#### 9.2 Gas

Based on the information provided by BeforeUDig, there are existing MP4 gas lines within the berms along Dominion Road and Valley Road. There are existing gas connections servicing the existing development, and therefore, we consider it is likely that the existing gas network will have adequate capacity to service the demands of the proposed development.

#### 9.3 Communications

Based on the information provided by Vector, there is existing underground communication and fibre infrastructure within proximity of the site. We consider that it is likely that the existing network will have adequate capacity to service the communications demands of the proposed development. However, this would need to be confirmed by a third-party service provider (Vector/Chorus) once the layout of the proposed development has been finalised.





### **10 SUMMARY AND CONCLUSIONS**

#### Earthworks

- 10.1 Bulk earthworks for the site are to be undertaken over an area of approximately 5,200 m<sup>2</sup> and cut and full volumes of approximately 3,000 m<sup>3</sup> and 1,300 m<sup>3</sup>, respectively and as such require resource consent under E12.4.1 of the AUP.
- 10.2 Bulk earthworks will involve excavating generally up to 1.0 m depth, and locally up to 3.6m depth in the northwest corner. The excavation will mostly involve basalt rubble and rock, but some solid rock excavation using heavy equipment and rock breaking is likely to be required. Noise and vibration are to be managed in accordance with Marshall Day's Assessment of Acoustic Effects, 27 August 2024.
- 10.3 The fill and volcanic rubble and rock are low sediment generating materials. Erosion and sediment controls in accordance with Auckland Council's GD05 are to be implemented to mitigate adverse sediment effects and these will be monitored during construction via an Earthworks Construction Management Plan.

#### Stormwater

- 10.4 The impervious surfaces on the site are to be reduced from approximately 100% (5,250 m<sup>2</sup>) to approximately 81% (4,210 m<sup>2</sup>). As such, the proposed development is considered a Brownfield Small under the Auckland Council's NDC and also requires resource consent under E8.4.1 of the AUP.
- 10.5 Post-development primary (10 year) stormwater flows are reduced by 12% from predevelopment flows and are to be discharged via on-site ground soakage. Soakage testing has been undertaken at the site and preliminary soakage design undertaken in accordance with Auckland Council's GD07 and this indicates sufficient soakage is readily available.
- 10.6 Post-development secondary (100 year) flows are reduced by 7% from the pre-development flows and are to be directed to the adjacent road carriageway on Valley Road in accordance with the Auckland Council's Stormwater Code of Practice.
- 10.7 As a result of the above, there will no increase in nuisance or damage to other properties during 10% (10 year) or 1% AEP (100 year) rainfall events. Also, refer to separate Babbage Flood Report.
- 10.8 Stormwater quality treatment in accordance with Auckland Council's GD01 is proposed for the uncovered vehicle pavements in the eastern area of the site prior to discharge to the on site soakpits.





#### Wastewater and Water Supply

- 10.9 The peak wastewater flows from the proposed development have been assessed against the capacity of the existing public network which indicates the public network has sufficient capacity for the proposed development.
- 10.10 The peak potable water demand from the proposed development has been assessed against the layout and size of the existing public network which indicates the public network is expected to sufficient capacity for the proposed development.
- 10.11 The firefighting water demand from the proposed development has been assessed against the layout and size of the existing public network which indicates the public network is expected to sufficient capacity for the proposed development subject to flow and pressure testing of the existing public network.

#### **Utility Services**

10.12 There are existing power supply, telecommunication and gas networks within the berms of Dominion Road and Valley Road and these are likely to have sufficient capacity to meet the demands of the proposed development subject to confirmation form the utility asset owners.





### **APPLICABILITY AND LIMITATIONS**

#### **Restrictions of Intended Purpose**

This report has been prepared solely for the benefit of Precinct Properties New Zealand Limited as our client with respect to the brief. The reliance by other parties on the information or opinions contained in the report shall, without our prior review and agreement in writing, be at such party's sole risk.

#### **Legal Interpretation**

Opinions and judgements expressed herein are based on our understanding and interpretation of current regulatory standards, and should not be construed as legal opinions. Where opinions or judgements are to be relied on they should be independently verified with appropriate legal advice.

#### Maps and Images

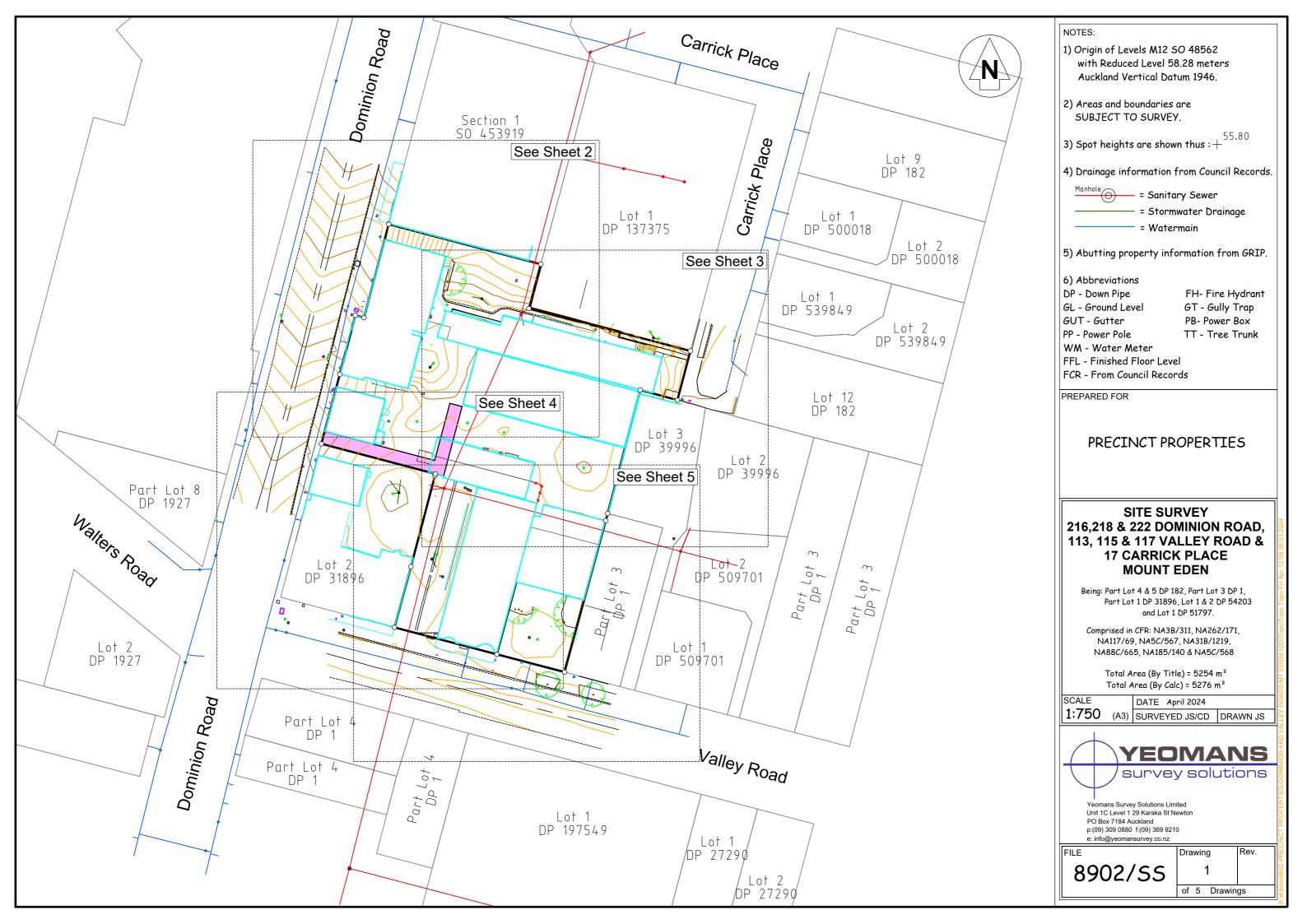
All maps, plans, and figures included in this report are indicative only. Do not scale any of the maps, plans or figures in this report. Sources for map and plan compositions include LINZ Data and Map Services and local council GIS services.

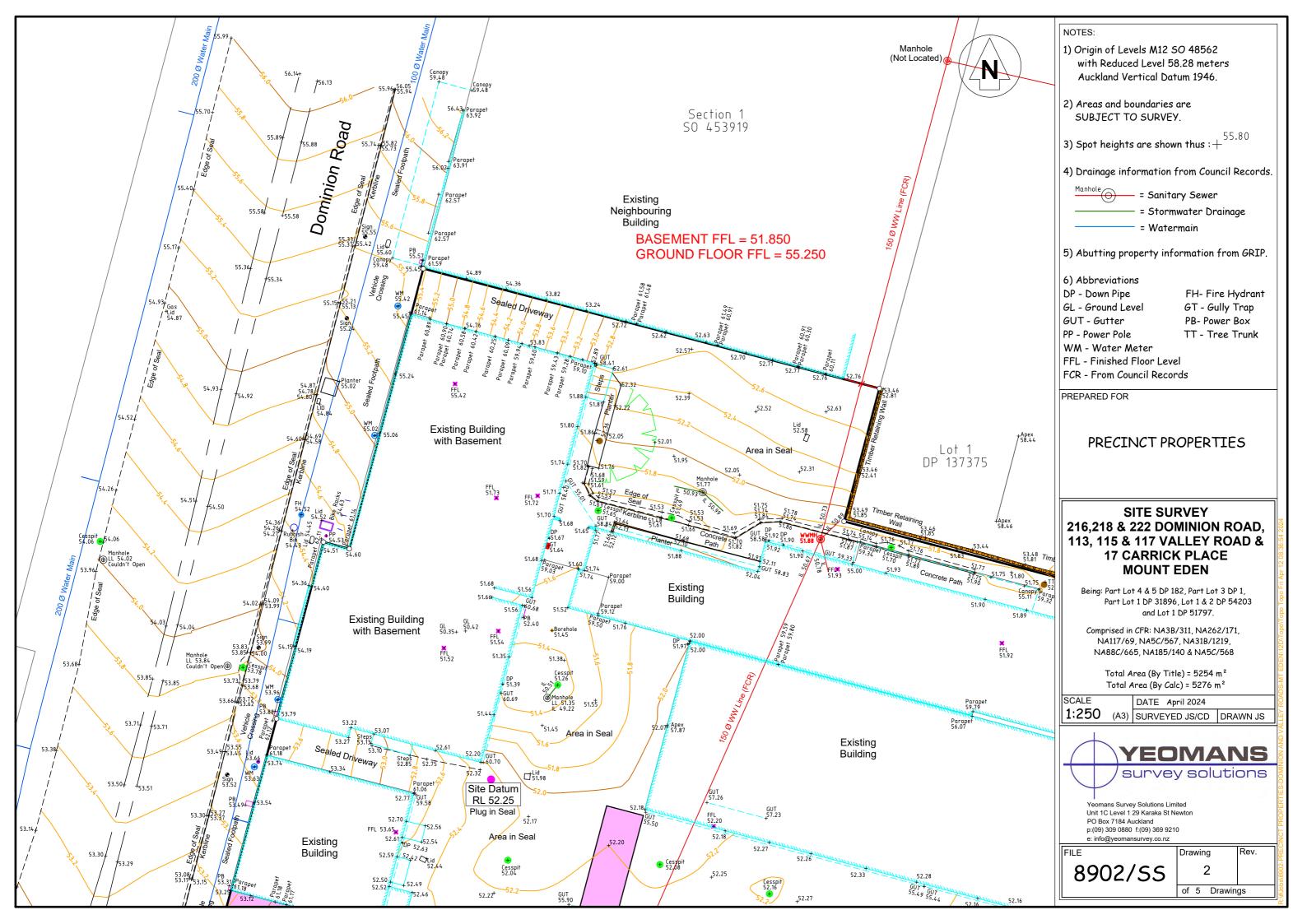


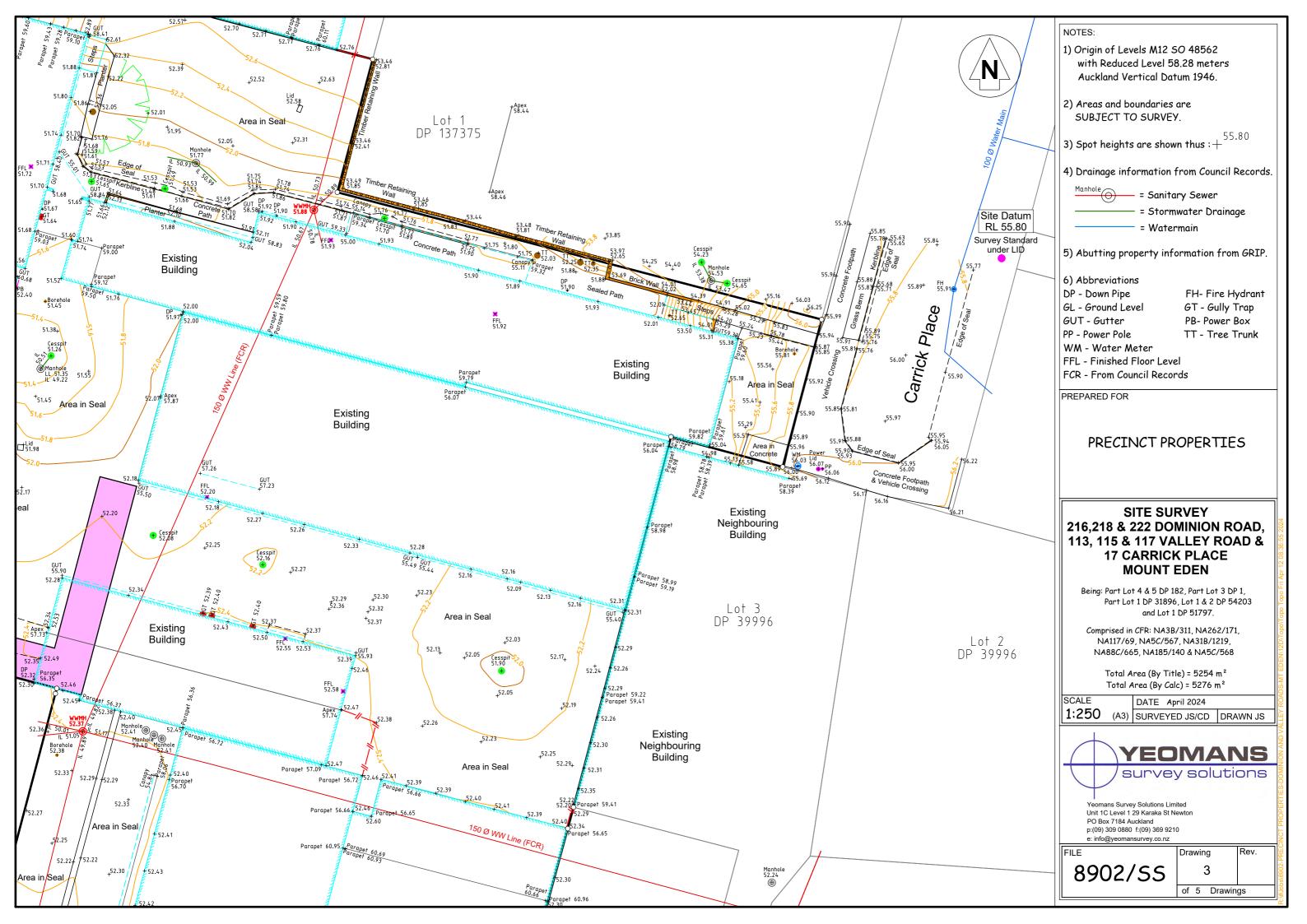


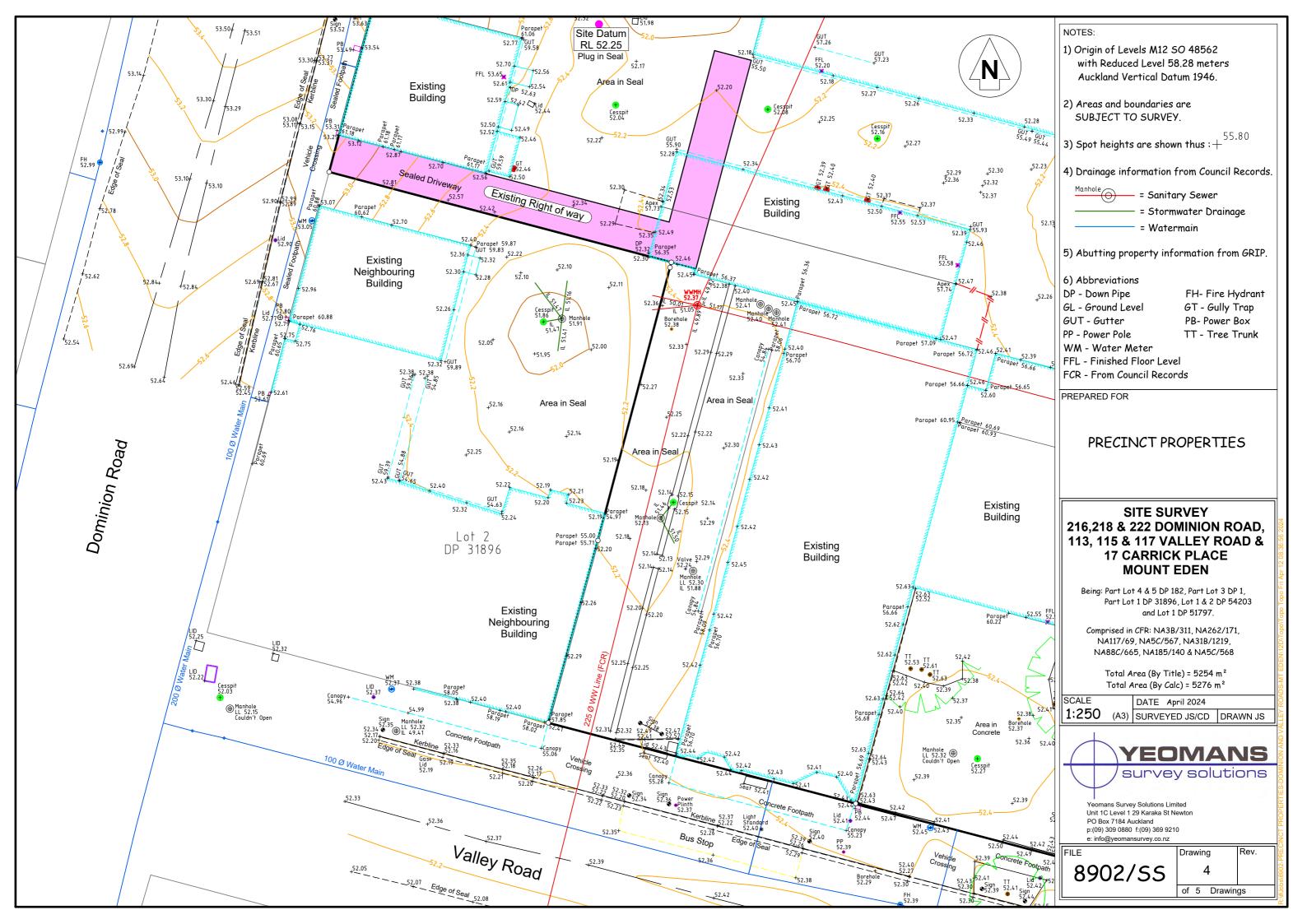
Appendix A Topographical Survey

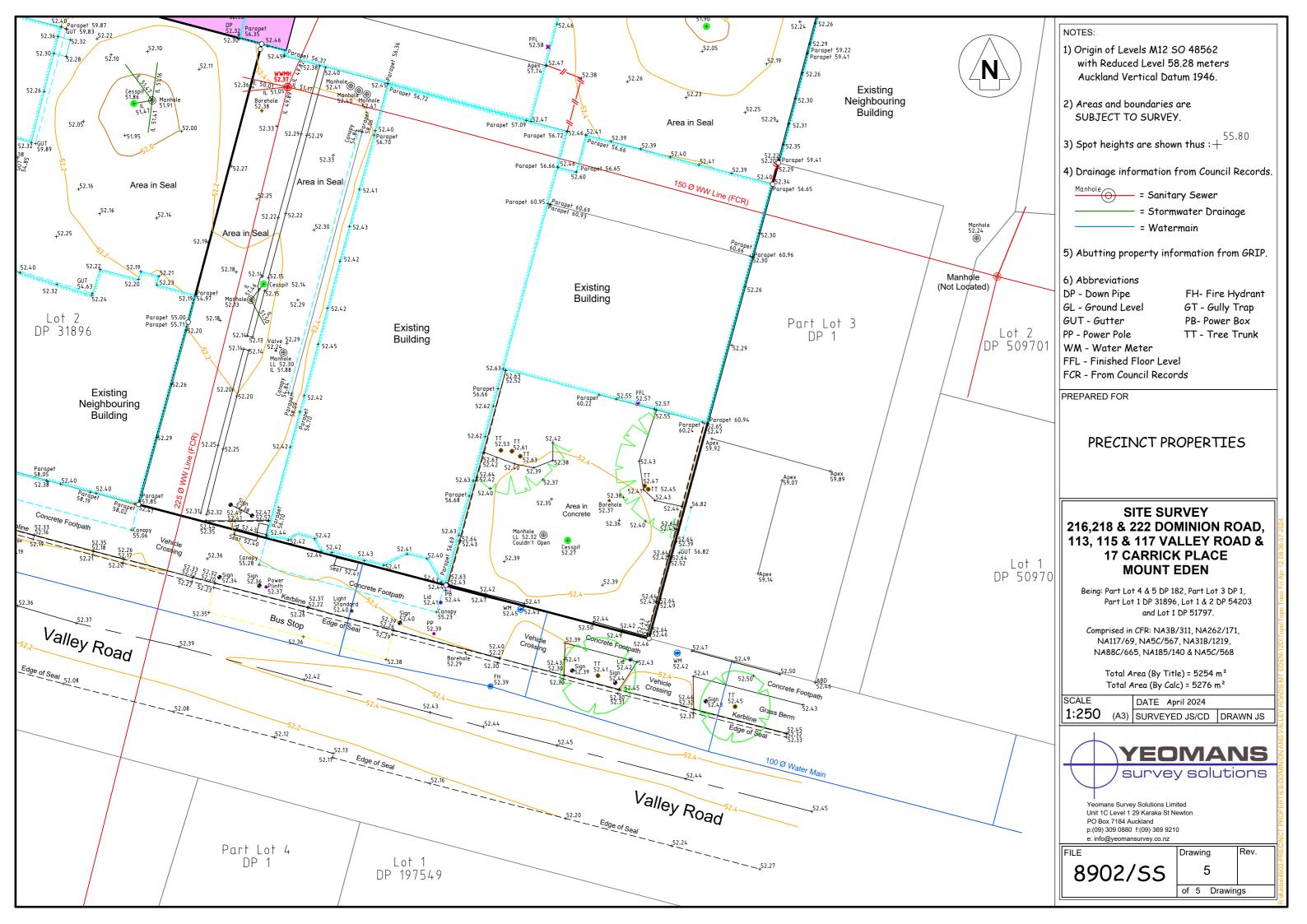










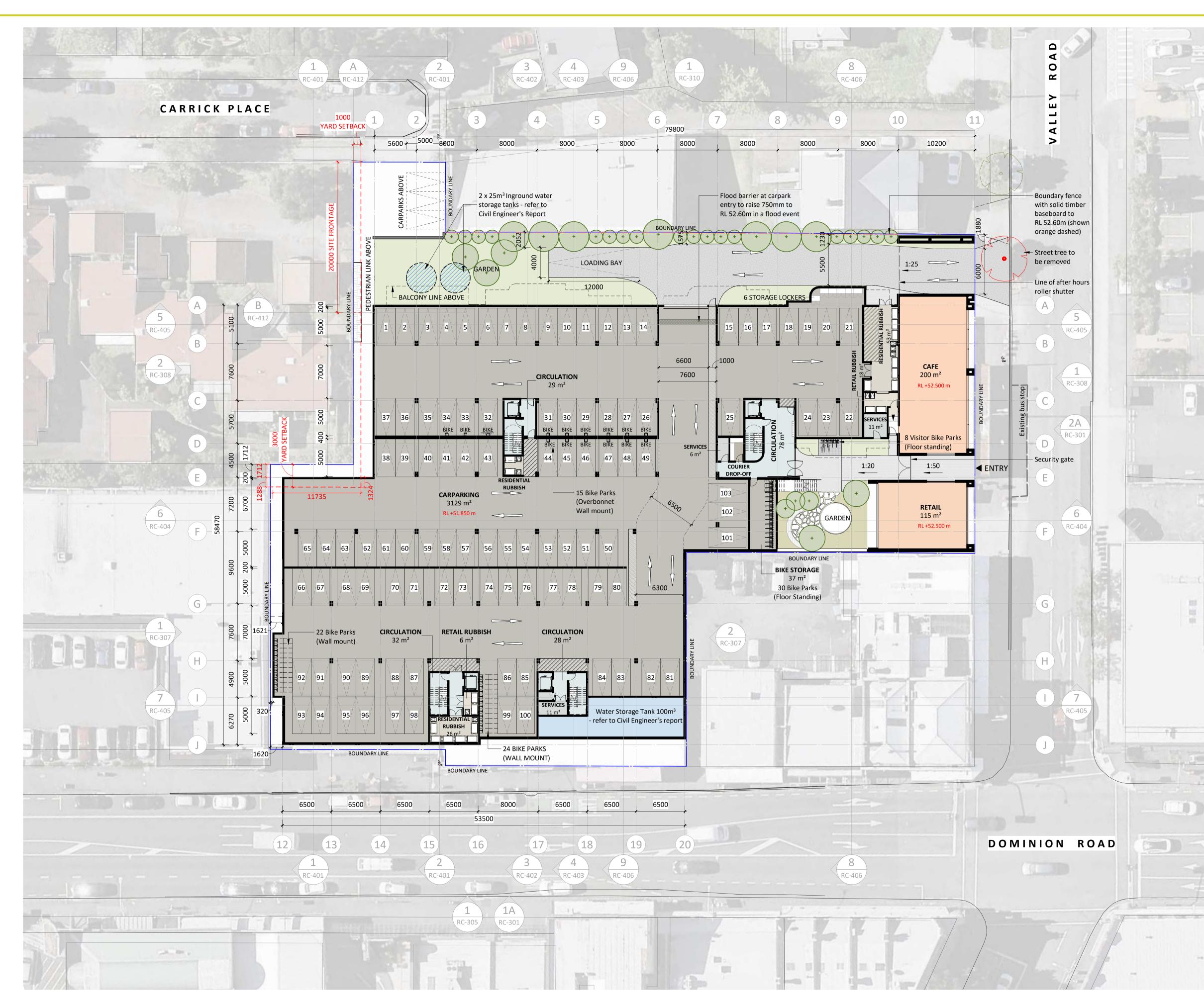




### **Appendix B**

**Proposed Development Layout** 





ashtonmitchell 



PROPOSED PLAN - LEVEL O

## 1:250

### COLOUR LEGEND

RETAIL
CAFE
CARPARKING
CIRCULATION
COURIER DROP-OFF
BIKE STORAGE
RESIDENTIAL RUBBISH
RETAIL RUBBISH
SERVICES
WATER STORAGE

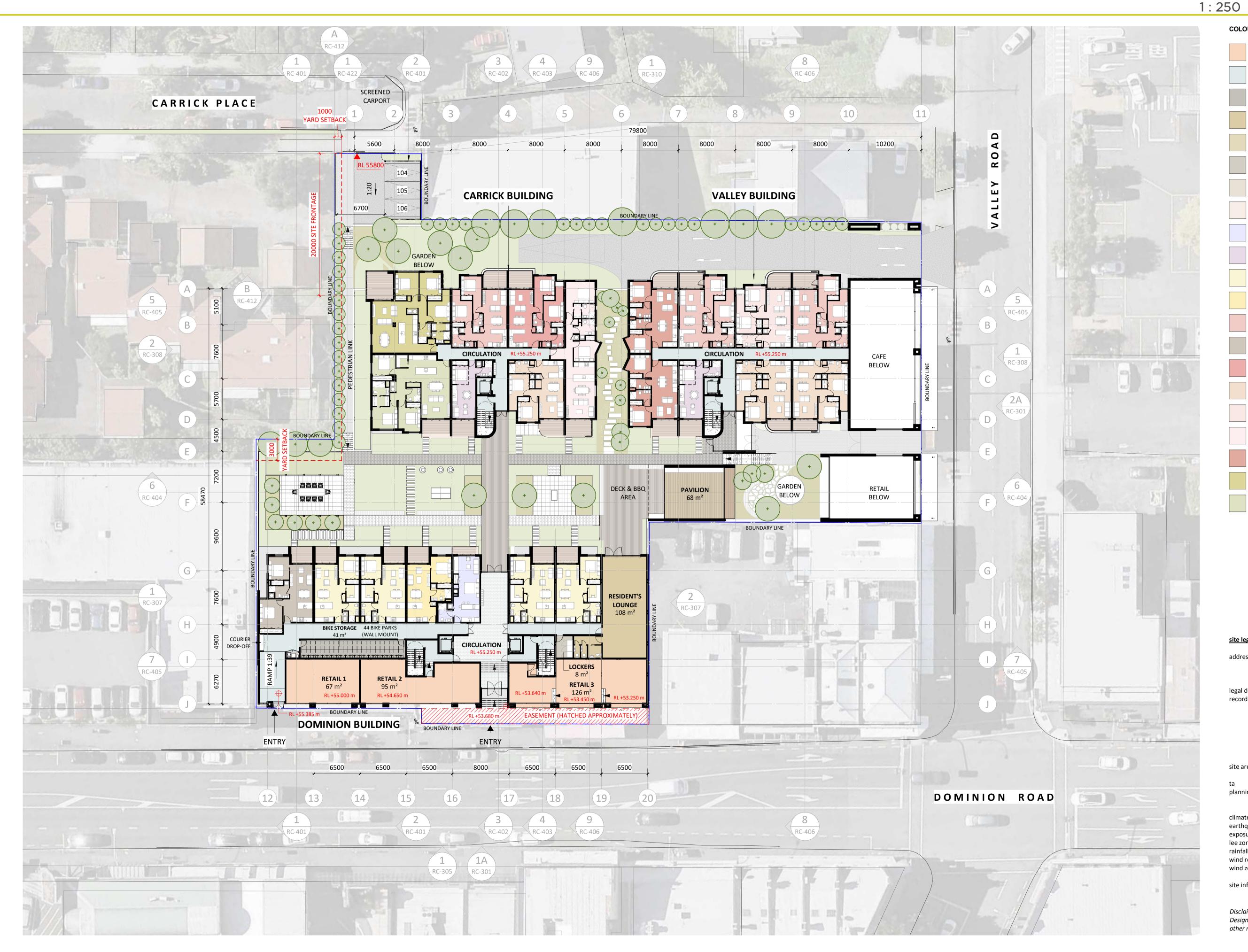
address	113-117 Valley Road, Mt Eden 198-202 Dominion Road, Mt Eden
	214-222 Dominion Road, Mt Eden
legal description,	Lot 1 DP 54203, NA5C/568
record of title number	Pt Lot 3 DP 1, NA185/140
	Pt Lot 3 DP 1, NA88C/665
	Pt Lot 3 DP 1, NA31B/1219
	Lot 1 DP 51797& Pt Lot 4 DP 182, NA3B/31
	Pt Lot 5 DP 182, NA262/171
	Lot 2 DP 54203 & Pt Lot 1 DP 31896, NA5C,
	Pt Lot 3, Allot 8, Sec10, NA117/69
site area	5173m2
ta	Auckland Council
planning zone	Business - Local Centre
	Residential - Terrace Housing
	and Apartment Buildings (THAB)
climate zone	1
earthquake zone	1
exposure zone	C
lee zone	No
rainfall intensity	80-90
wind region	A
wind zone	Low

Disclaimer: Design subject to verification by Structural Engineer and other relevant consultants.





job:



ashtonmitchell 



PROPOSED PLAN - LEVEL 1

# COLOUR LEGEND RETAIL CIRCULATION BIKE STORAGE RESIDENT'S LOUNGE PAVILION LOCKERS RETAIL RUBBISH BALCONY TYPE S4 - 1 BEDROOM STUDIO TYPE S6 - 1 BEDROOM STUDIO TYPE 1A - 1 BEDROOM + MULTI TYPE 1C - 1 BEDROOM + 1 BATHROOM TYPE 2A - 2 BEDROOM + 2 BATHROOM TYPE 2E - 2 BEDROOM + 1 BATHROOM (END) TYPE 2J - 2 BEDROOM + 2 BATHROOM TYPE 2L - 2 BEDROOM + 1 BATHROOM TYPE 2P - 2 BEDROOM + 1 BATHROOM TYPE 2X - 2 BEDROOM + 2 BATHROOM TYPE 2Y - 2 BEDROOM + 2 BATHROOM TYPE 3A - 3 BEDROOM (END)

TYPE 3B - 3 BEDROOM (END)

### <u>site legend</u>

address	113-117 Valley Road, Mt Eden
	198-202 Dominion Road, Mt Eden
	214-222 Dominion Road, Mt Eden
legal description,	Lot 1 DP 54203, NA5C/568
record of title number	Pt Lot 3 DP 1, NA185/140
	Pt Lot 3 DP 1, NA88C/665
	Pt Lot 3 DP 1, NA31B/1219
	Lot 1 DP 51797& Pt Lot 4 DP 182, NA3B/311
	Pt Lot 5 DP 182, NA262/171
	Lot 2 DP 54203 & Pt Lot 1 DP 31896, NA5C/567
	Pt Lot 3, Allot 8, Sec10, NA117/69
site area	5173m2
ta	Auckland Council
planning zone	Business - Local Centre
	Residential - Terrace Housing
	and Apartment Buildings (THAB)
climate zone	1
earthquake zone	1
exposure zone	C
lee zone	No
rainfall intensity	80-90
wind region	A
wind zone	Low
oito information abtain	ad from CooNtons & DDANIZMons

site information obtained from GeoMaps & BRANZMaps

Disclaimer: Design subject to verification by Structural Engineer and other relevant consultants.



project name:



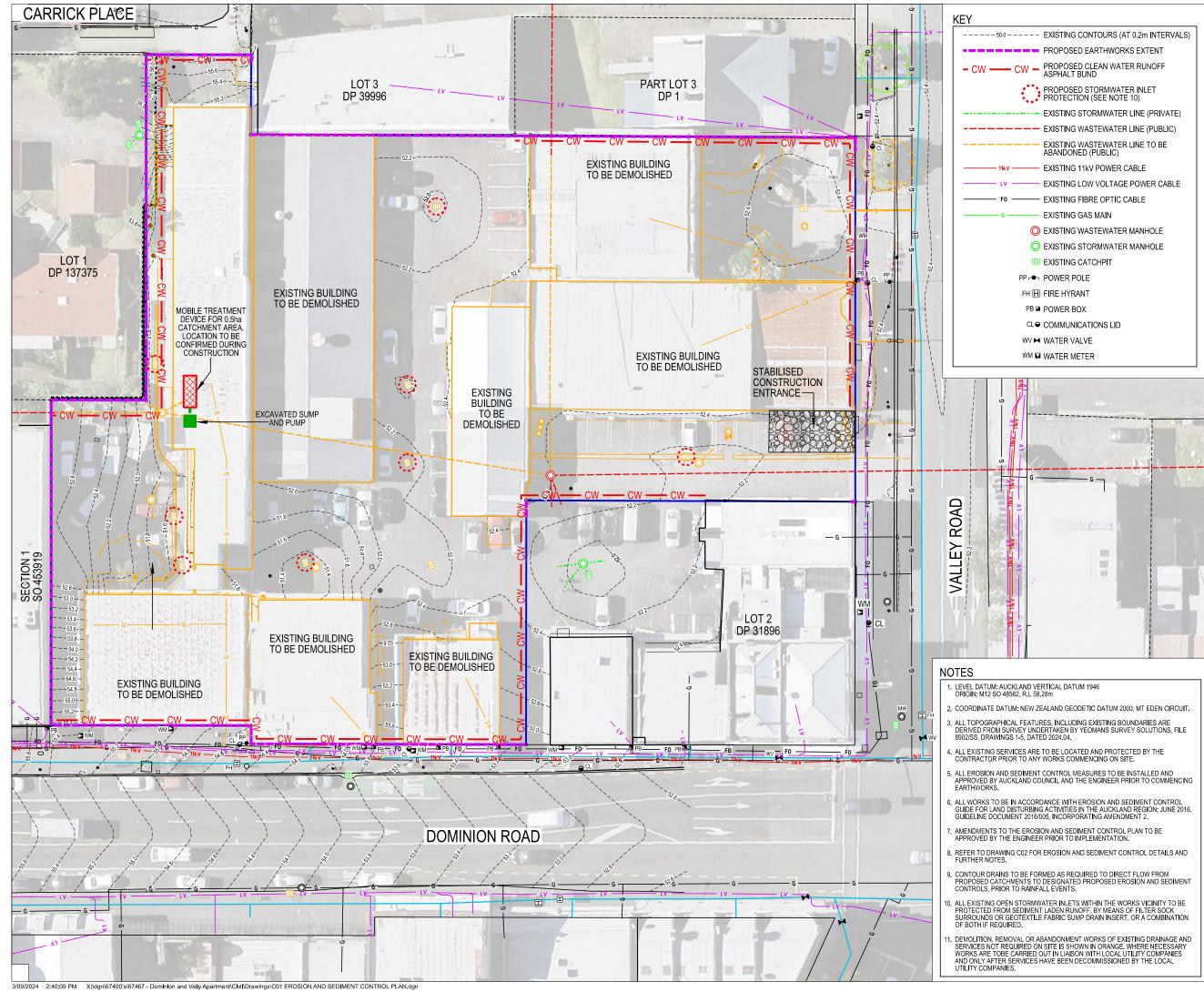
job:





Appendix C Civil Engineering Drawings





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DRAWING REVISIONS

DESCRIPTION

REV



DATE DRN DES APP BY CHK

PROJECT TITLE : DOMINION AND VALLEY APARTMENT

PRECINCT PROPERTIES RESIDENTIAL

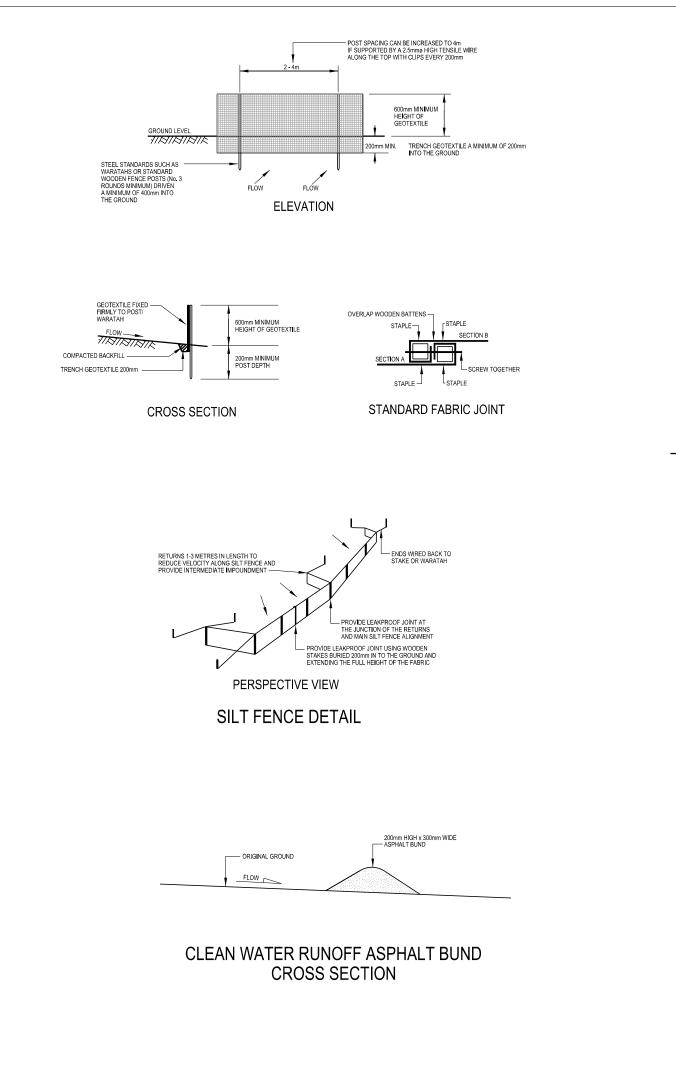
216 - 222 DOMINION ROAD MOUNT EDEN

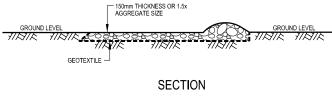


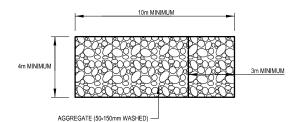
DRAWING TITLE: ERPSION AND SEDIMENT CONTROL PLAN

### FOR RESOURCE CONSENT 2024.09.03

2024.09.03			
	DATE	INITIAL	
DESIGNED	2024.08.30	JL	
DRAWN	2024.08.30	MJD	
DESIGN CHECK	2024.09.02	JC	
DRAWING CHECK	2024.09.02	MJD	
APPROVED	2024.09.02	MJM	
1:200 @ A1 1:400 @ A3			
JOB NO:			
67467			
DWG NO:		REV:	
C01		-	

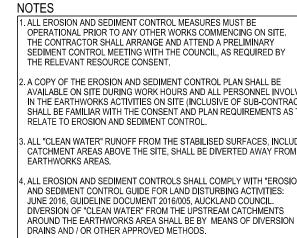






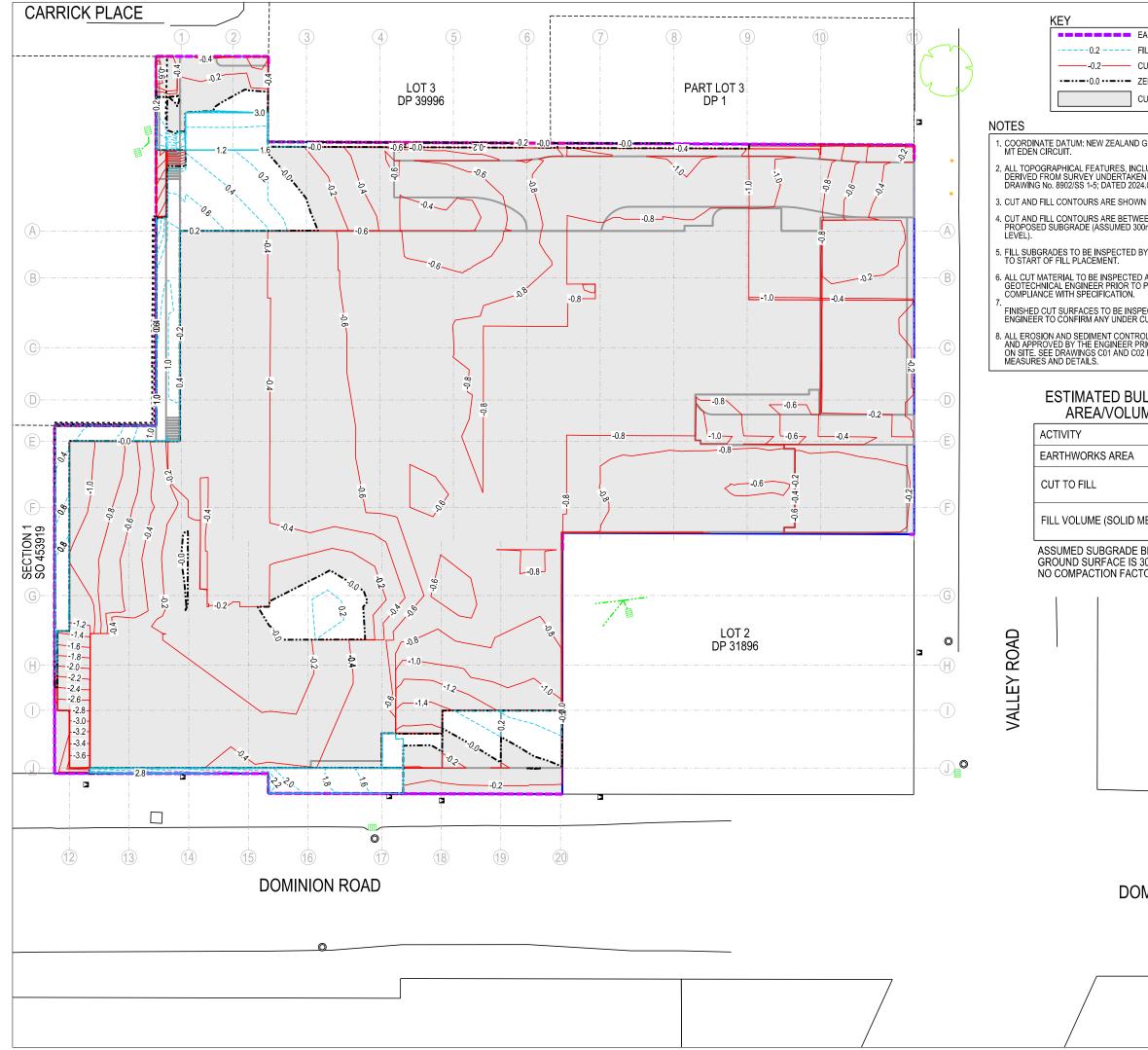
PLAN

## STABILISED CONSTRUCTION ENTRANCE

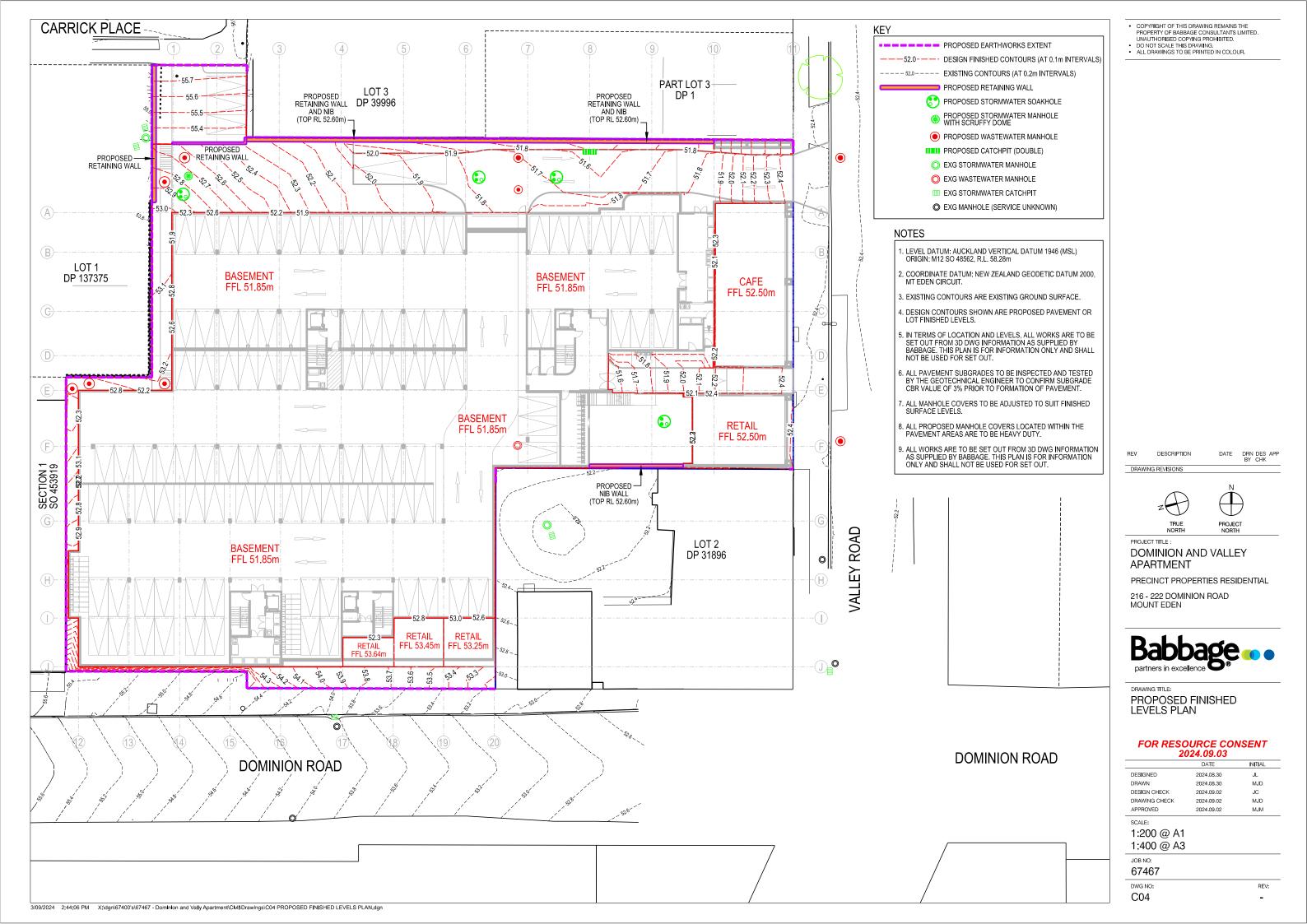


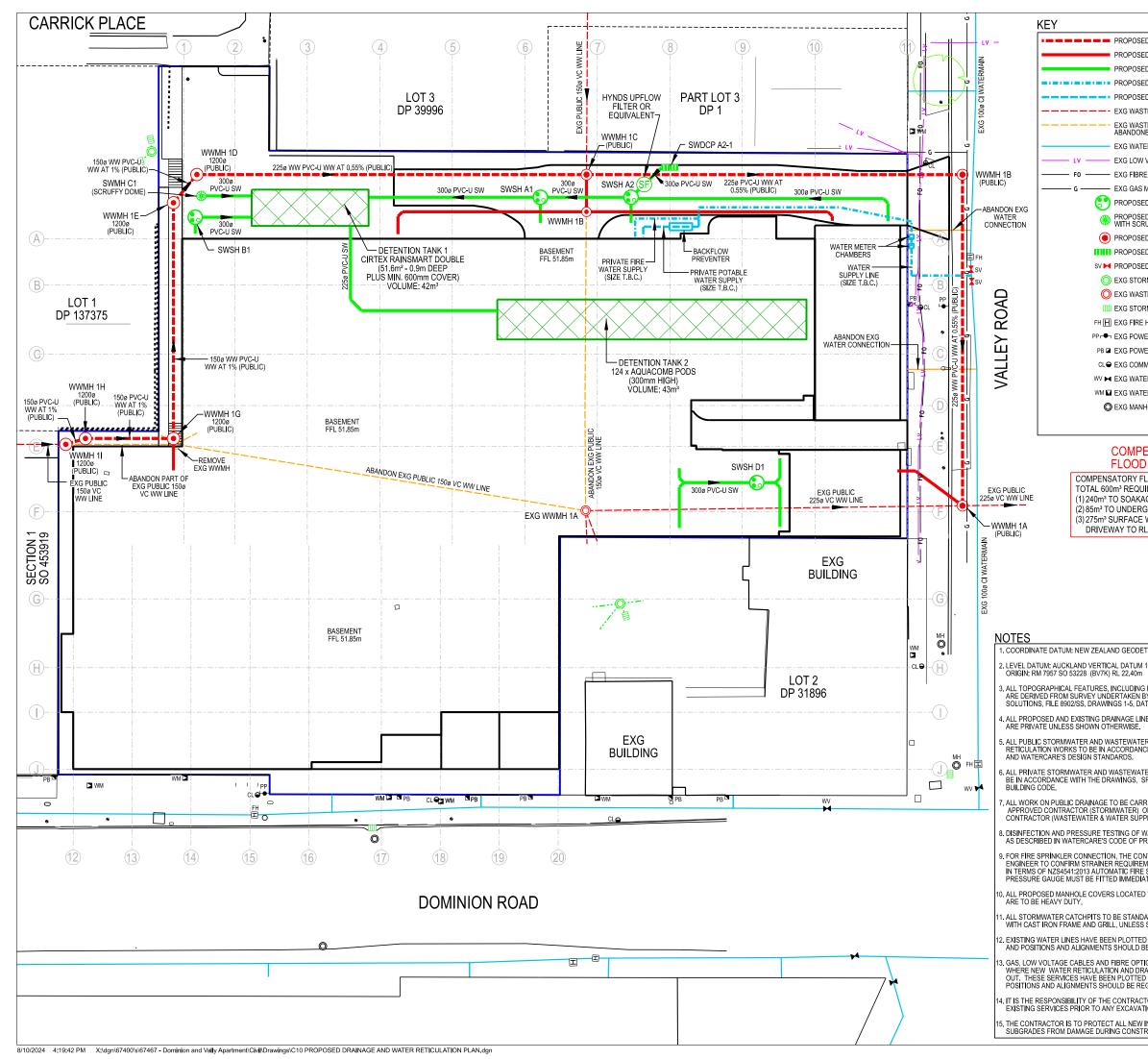
5. FURTHER SEDIMENT CONTROL WORKS MAY BE REQUIRED BY THE ENGINEER AS THE PROJECT ADVANCES. THESE WILL BE INSTALLED AS AND WHERE REQUIRED BY THE ENGINEER. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR ENSURING THAT THE SITE HAS EFFECTIVE EROSION AND SEDIMENT CONTROL MEASURES OPERATING AT ALL TIM

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Appendix D

**Stormwater Calculations** 



JOB NAME:	Domion & Valley Road	DATE: 15/08/2024	
			Dabbada
JOB NO:	67467#C	DES BY: MJM	Babbage ••••
			partners in excellence <b>O</b> ®
SUBJECT:	SW runoff calculations	CHKD BY:	

#### **TP108 RUNOFF CALCULATIONS**

#### **<u>1. PRE-DEVELOPMENT CATCHMENT (ASSUMED FULLY PERVIOUS):</u>**

Impervious Area	ha	0.5249
Pervious Area	ha	0.0025
Hydrological Soil Group		Group_A
SCS Curve Number (CN)		39
total area	ha	0.5274
% Impervious		100%
Catchment Slope (S <sub>c</sub> )	0.01	
Catchment Length (I)	m	100
Channelisation Factor (C)		0.6
Weighted Curve Number	97.7	
Initial Abstraction (Ia) weighted	0.024	
$t_c$ (For q* - TP108 Fig. 5.1)	hours	0.17
t <sub>p</sub> (SCS Lag for HEC-HMS)	hours	0.11
Storage (S) Total	mm	5.9

Table 3.3 - Curve numbers for typical Auckland conditions						
Land use	Group A Soil (volcanic granular loam)	Group B Soil (alluvial)	Group C Soil (mudstone/san dstone)			
Bush, humid-climate, not-grazed	30	55	70			
Pasture, lightly grazed, good grass cover	39	61	74			
Urban lawns	39	61	74			
Crops, straight rows, minimal vegetative cover	72	81	88			
Sealed roads, roofs	98	98	98			

INPUT VALUES

#### Apply Climate Change to Pre-development Scenario? Yes Select Yes or No

Select appropriate design storm		90th	2 yr ARI	10 yr ARI	100 yr ARI**	
24-Hour Rainfall Depth (P <sub>24</sub> )	mm	25	74.4	112	172	← NIWA HIRDS
24-hour rainfall depths with	mm	25	86	131	228	Refer Stormwater Code of Practice - Table 2
climate change allowances (P <sub>24</sub> )						
c*=(P24-2Ia)/(P24-2Ia+2S)		0.678	0.878	0.917	0.951	
q* (from Fig. 5.1)		0.149	0.160	0.161	0.164	SWCoP - Changes to normalised rainfall profile
Peak Flowrate (q <sub>p</sub> )	l/s	19.6	81.0	119.3	218.8	(Increased q <sub>p:</sub> 12% (2yr), 7% (10 yr), 11% (100yr))
24 hour rainfall depth (Q <sub>24)</sub>	mm	20.19	80.07	125.35	222.44	
24 hour runoff volume (V24)	m <sup>3</sup>	106.467	481.403	694.135	1184.906	(Increased V24: 14% (2yr), 5% (10 yr), 1% (100y

#### 2. POST-DEVELOPMENT CATCHMENT:

Impervious Area	ha	0.4274
Pervious Area	ha	0.1000
Hydrological Soil Group		Group_A
SCS Curve Number (CN)		39
total area	ha	0.5274
% Impervious		81%

Catchment Slope (S <sub>c</sub> )	m/m	0.02
Catchment Length (I)	m	100
Channelisation Factor ( C )		0.6
Weighted Curve Number		86.8
Initial Abstraction (Ia) weighted	mm	0.948
t <sub>c</sub> (For q* - TP108 Fig. 5.1)	hours	0.17
t <sub>p</sub> (SCS Lag for HEC-HMS)	hours	0.11
Storage (S) Total	mm	38.6

Roof	Imperv	0.3258 ha	
Pavement	Imperv	0.1016 ha	
Favement	imperv	0.1010 11a	
Landscape	Pervious	0.1 ha	
		0.5274 ha	

# Auckland Council - Stormwater Code of Practice V4 - Climate Change

Table 1: Percentage Increase in 24-hour Design Rainfall Depth								
AEP	50%	20%	10%	5%	2%	1%		

ARI	2 yr	5 yr	10 yr	20 yr	50 yr	100 yr
% Increase *	15.1%	16.4%	17.0%	17.2%	17.6%	32.7%

 \* in 24-Hour Design Rainfall Depth Due to Future Climate Change assuming 2.1°C increase in temperature

\*\* SWCoP V4 requires 3.8°C Climate Change allowance for 1% AEP event

Select appropriate design storm	•	90th	2 yr ARI	10 yr ARI	100 yr ARI**	
24-Hour Rainfall Depth (P <sub>24</sub> )	mm	25	74.4	112	172	← NIWA HIRDS
24-hour rainfall depths with climate change allowances (P <sub>24</sub> )	mm	25	86	131	228	Refer Stormwater Code of Practice - Table 1
c*=(P24-2Ia)/(P24-2Ia+2S)		0.230	0.520	0.626	0.746	
q* (from Fig. 5.1)		0.067	0.127	0.143	0.152	SWCoP - Changes to normalised rainfall profile:
Peak Flowrate (q <sub>p</sub> )	l/s	8.9	64.4	105.4	202.6	(Increased q <sub>p:</sub> 12% (2yr), 7% (10 yr), 11% (100yr))
24 hour rainfall depth (Q <sub>24)</sub>	mm	9.24	58.18	100.33	194.31	
24 hour runoff volume (V24)	m <sup>3</sup>	48.711	349.798	555.623	1035.050	(Increased V24: 14% (2yr), 5% (10 yr), 1% (100yr)

Note: Calculation based on homogeneous catchment (impervious and pervious areas discharge to same network or flowpath) using weighted curve number (CN) and combined 24 hour rainfall depth and volume (refer ARC TP108, Sections 3.2 and 4.2)



Appendix E Soakage Testing





Job No: 30717 4 November 2016

Panuku Development Auckland c/- Beca PO Box 6345 Wellesley Street Auckland 1141

Attention: Anne Maree O'Connor

Dear Anne Maree

## 216-222 Dominion Road & 113-117 Valley Road, Mt Eden Soakage Investigation

### 1 Introduction

Tonkin & Taylor Ltd (T+T) was engaged by Panuku Development Auckland to provide geotechnical advice and undertake soakage testing of rock bore soakholes on the subject site at 216-222 Dominion Road and 113-117 Valley Road, Mt Eden, Auckland. The work was undertaken as an extension to our existing contract, with an approval to proceed on 25 October 2016 from the project manager, Beca<sup>1</sup>.

This letter summarises the soakage investigation drilling work and the results of the soakage flowrate testing within the boreholes. We understand that this information will be used in support of a response to a Section 92 request from Auckland Council for Resource Consent for the proposed development at the subject site. Stormwater from the proposed apartment building development is to be disposed using soakholes in the basalt rock.

### 2 Soakage Investigation

We understand that as part of the consenting process, Auckland Council has queried the soakage borehole capacity of 50 L/s initially proposed by Beca civil engineers, and have requested that specific test results be provided to justify the assumed soakage capacity.

T+T have therefore undertaken soakage borehole drilling in two locations across the subject site in order to confirm the available soakage flow rates. Boreholes were drilled inclined from vertical (approx. 10°) in order to increase the likelihood of the holes intersecting vertical cooling joints that are characteristic of the basalt rock. Increased soakage capacity is usually available in jointed basalt compared to massive rock.

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<sup>&</sup>lt;sup>1</sup> Beca, 2016, Email correspondence from Anne Maree O'Connor "RE: Soakage Investigation – Dominion/Valley Road", dated 25/10/2016, 10.50am.

Exceptional thinking together

The two boreholes were drilled by Intorock Drilling Ltd on 1 November 2016 using percussion and down-hole hammer drilling methods. The upper 3m of each borehole was supported by a 90mm diameter PVC casing. Soakage testing (constant head test) was subsequently carried out in accordance with Auckland Council requirements<sup>2</sup>. Borehole 1 was drilled to a total inclined depth of 23.5m and soakage testing yielded a maximum soakage rate of 34.7 L/s over 10 minutes. Borehole 2 was drilled to a total inclined depth of 25.6m and soakage testing yielded a maximum soakage rate of 34.7 L/s over 10 minutes. The boreholes were pre-soaked prior to flow testing.

On the basis of the soakage testing, a typical flow rate of up to 35 L/s is considered appropriate for preliminary design of soakage for the proposed development. The adjusted flow rate allowing for a scaling factor of 1.3, is 26.9 L/s in accordance with the Auckland Council constant-head test worksheet.

The borehole locations are shown on the site plan attached in Appendix A. Drilling logs and flowrate testing results are presented in Appendix B. The constant-head test worksheet is presented in Appendix C.

## 3 Permanent Soakhole Design

The results of the soakage flow rate testing provide a reasonable basis for preliminary soakage design and consenting purposes. Given the significant thickness of basalt underlying the subject site, and the extensive use of soakage boreholes on other sites in the immediate vicinity of the project. It is expected that similar soakage rates will be available across the site. However, we note that basalt is typically variable in terms of porosity/voids and the orientation of joints or fractures in the rock that influence available soakage. It is therefore possible for soakage conditions to differ considerably over a short distance.

Therefore, we recommend that the permanent 'production' soakage boreholes be also drilled at a 10° incline (off vertical) to increase the likelihood of intersecting vertical rock fractures. We also recommend that flow rate testing be undertaken on those production soakage boreholes at time of installation, to prove their capacity exceeds the minimum flow rate required by the design. Should the production soakholes not achieve the required capacity, then other soakhole locations will need to be considered.

For further information and characterisation of site subsurface conditions, refer to the T+T geotechnical investigation report for the proposed development<sup>3</sup>.

## 4 Summary

On the basis of the soakage testing that has been carried out, we summarise the conclusions as follows:

- Soakage testing performed in boreholes 1 and 2 confirmed a soakage capacity of 34.7 L/s and 35.3 L/s respectively, each over a 10 minute duration.
- On the basis of the soakage testing, a typical capacity of up to 35 L/s is considered appropriate for preliminary design of soakage for the proposed development. The adjusted capacity for each soakhole, allowing for a factor of 1.3, is 26.9 L/s in accordance with the Auckland Council constant-head test worksheet.
- The permanent 'production' soakage boreholes should be drilled at a 10° incline to vertical to increase the likelihood of the boreholes intersecting vertical rock fractures.

<sup>&</sup>lt;sup>2</sup> Auckland Council, 2013, *Stormwater Disposal via Soakage in the Auckland Region*. Technical Report 2013/040, dated October 2013.

<sup>&</sup>lt;sup>3</sup> T+T, 2016, Geotechnical consultancy services: Valley Road Apartments – Mt Eden. Ref 30717.001v2, dated May 2016.

• Flow rate testing should be undertaken on the production soakage boreholes at the time of installation, to prove their capacity exceeds the minimum flow rate required by design. If the design capacity cannot be demonstrated, replacement or supplementary soakholes may be required.

#### 5 Applicability

This report has been prepared for the exclusive use of our client Panuku Development Auckland, and Auckland Council, with respect to the particular brief given to us and it may not be relied upon in other contexts or for any other purpose, or by any person other than our client, without our prior written agreement.

**Tonkin & Taylor Ltd** 

**Environmental and Engineering Consultants** 

Report prepared by:

Authorised for Tonkin & Taylor Ltd by:

Joshua Teal

**Geotechnical Engineer** 

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Robert Hillier Project Director

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# Appendix F

Water and Wastewater Calculations



JOB NAME:	Dominion & Valley Road Apartmen	ts DATE:	: 30/08/2024 <b>Babbado</b>
JOB NO:	67467#C	DES BY:	Babbage • •
SUBJECT:	Wastewater Flows	СНКД ВҮ:	: JL

Residential Wastewater Flows											
Catchment ID	No. of Dwellings	Bedrooms	Occupancy	Design Wastewater Flow Allowance	Daily Discharge	Peak Dry Weather Flow (PDWF)		Peak Wet Weather Flow (PWWF)			
						Peaking Factor	PDWF	Peaking Factor	PWWF		
				L/p/day	L/day		L/s		L/s		
1 Bed Apartments	43	1	2.0	180	15480	3.0	0.54	5.0	0.90		
2 Bed Apartments	81	2-4	3.0	180	43740	3.0	1.52	5.0	2.53		
3 Bed Apartments	11	2-4	3.0	180	5940	3.0	0.21	5.0	0.34		
Totals	135				65160		2.26		3.77		

Residential wastewater design flows have been calculated according to Water and Wastewater

Code of Practice for Land Development and Subdivision, Chapter 5, Section 5.3.5.1.1

Commercial Wastewater Flows										
Catchment ID	Area	Occupancy	Design Wastewater Flow Allowance	Design Wastewater Flow Allowance	Daily Discharge	Peak Dry Weather Flow (PDWF)		Peak Wet Weather Flow (PWWF)		
						Peaking Factor	PDWF	Peaking Factor	PWWF	
	m²	1 person/m <sup>2</sup>	L/day/m <sup>2</sup>	L/p/day	L/day		L/s		L/s	
Wet retail (café)	200	50	N/A	65	260	2.0	0.01	5.0	0.02	
Dry retail	115	N/A	15	N/A	1725	2.0	0.04	6.7	0.13	
Totals	315				1985		0.05		0.15	

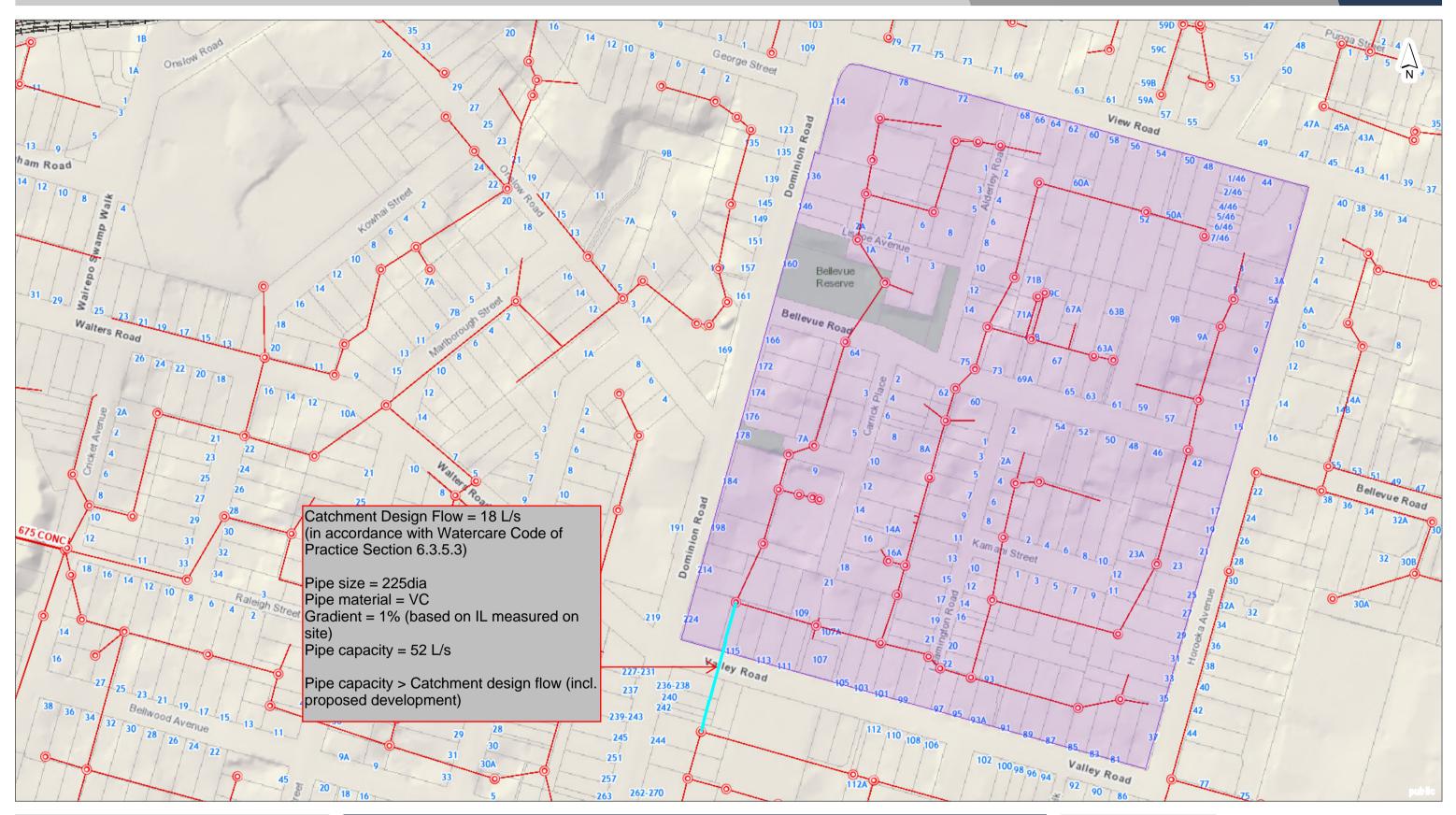
Commercial wastewater design flows have been calculated according to Water and Wastewater

Code of Practice for Land Development and Subdivision, Chapter 5, Section 5.3.5.1.1

	Daily
	Discharge
	L/day
Totals	67145

PWWF
L/s
3.92

# **Auckland Council**



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**Dominion and Valley - WW Assessment** 

# Мар



Scale @ A3 = 1:2,500

**Date Printed:** 3/09/2024





JOB NAME:	Dominion & Valley Road Apartment	DATE: 3/09/2024	Babbage •••
JOB NO:	67467#C	DES BY: WD	
SUBJECT:	Potable Water Supply Demand	CHKD BY: MJM	

Residential Water Demand										
Catchment ID	No. of Dwellings	Bedrooms	Occupancy	Design Water Flow Allowance	Average Daily Demand	Peak Daily Demand (PDD)		Peak Hourly Demand (PHD)		
						Peaking Factor	PDD	Peaking Factor	PHD	
	m2			L/p/day	L/day		L/day		L/s	
1 Bed Apartments	43	1	2.0	200	17200	2.0	34400	2.5	1.00	
2 Bed Apartments	81	2-4	3.0	200	48600	2.0	97200	2.5	2.81	
3 Bed Apartments	11	2-4	3.0	200	6600	2.0	13200	2.5	0.38	
Total	135				72400		144800		4.19	

from Water and Wastewater Code of Practice for Land Development

and Subdivision, Chapter 6, Table 6.1.a

			Commercial	Water Dema	and				
Catchment ID	Area 1	No. of People	Design Water Flow Allowance	Design Water Flow Allowance	Average Daily Demand	Peak Daily Demand (PDD)		Peak Hourly Demand (PHD)	
						Peaking Factor	PDD	Peaking Factor	PHD
	m2		L/m2/day	L/p/day	L/day		L/day		L/s
Wet retail (café) Dry retail	200 115	N/A 2.3	15 N/A	N/A 65	3000 150	2.0 2.0	6000 299	2.5 2.5	0.17 0.01
Total	315				3150		6299		0.18

from Water and Wastewater Code of Practice for Land Development

and Subdivision, Chapter 6, Table 6.1.c

	Average Daily Demand	PDD	PHD
	L/day	L/day	L/s
Totals	75550	151099	4.37